

Dipartimento di Fisica





Polarization issues for CMB devices

Scientific target

Cosmic Microwave Background Polarization B modes

Experimental aspects

QUBIC (Q & U Bolometric Interferometry for Cosmology) experiment

Shields analysis with GRASP

Anti Reflection Structures (ARS)

ARS

CMB Polarisation

Differently by CMB temperature anisotropy, the polarization is generated only by scattering; when we observe the polarization we are looking directly at the so-called last scattering surface (LSS) of the photons direct probe of the Universe at the epoch of recombination

• CMB Polarisation is due to the Thomson scattering of the radiation pattern at the recombination

To obtain a net linear polarized signal, a local temperature quadrupole anisotropy pattern in the primordial plasma is needed





• <u>Scalar Perturbations</u>: density perturbations in the plasma **provide** symmetric quadrupole

(Compression)

Scalars

Scalars

Vectors

Vector

(Vorticity)

Tensors

(Gravity Waves)

Tensor

• Vector Perturbations: vorticity in the plasma (negligible @ recombination)

hot

• <u>Tensor Perturbations</u>: due to gravitational waves that stretch and squeeze space and λ of the CMB photons asymmetric quadrupole polarization pattern "<u>handedness</u>"



ARS

CMB Polarisation

Why we want to measure B modes?

- <u>Scalar perturbations</u> (density fluctuations) only E modes
 Fluctuations we observe today originated from quantum fluctuations generated during inflation
- 1 Tensor perturbations (gravitational waves) both E and B modes
 Gravitational waves originated from quantum fluctuations generated during

inflation

Detection of the B modes in CMB polarization pattern is the Holy Grail for Cosmology

B modes are the smoking gun for Inflation theory Measure of the tensor to scalar ratio at the energy scale of Inflation



 $V^{\frac{1}{4}} = 1.06 \times 10^{16} GeV(\frac{r_{ij}}{0.01})^{\frac{1}{4}}$

Interferometer vs Imager

Actual instrumental techniques to measure B modes

VS



CMB



ARS

- **INTERFEROMETERS**(CBI, DASI Interferometer)
- better control of the systematics
- no telescope low ground pick-up and cross polarization
- angular resolution defined by antennas positions
- Iimited number of channels and amplifier
- noise

Observing the Universe with the Cosmic Microwave Background, 22-26 April 2014, L'Aquila, Dr. Daniele Buzi **IMAGERS** (BICEP, EBEX, SPIDER, QUITE, PolarBear)

- good sensitivity thanks to large bolometers arrays (wide band, low noise)
- systematics induced by telescope's presence
- angular resolution defined by antennas positions
- atmospheric noise accurate scan strategy

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CMB Polarisation

QUBIC

Conclusions

CMB Polarisation

A new technique that combines the advantages of the interferometers in terms of control of the systematics with high sensitivity of cryogenic bolometers

BOLOMETRIC INTERFEROMETRY

ARS



Measurement of the **Visibilities** that are the FT of the observed CMB sky field (C_{2} CMB power spectrum is directly the square modulus of the visibilities)

Each bolometer measures the total power given by the sum of the radiation incoming from all antennas (Fizeau Interferometer) $<(E_1 + E_2)^2 > = < E_1^2 > + < E_2^2 > + 2 < E_1E_2^* >$

Each bolometer measures linear combinations of all Stokes parameters I, Q and U

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Q & U Bolometric Interferometry for Cosmology







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Constrain the B-modes down to r=0.01 @ 95% of confidence level

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ARS

Dome C

Conclusions

Hobart

Mario Zucchelli

Christchurch

QUBIC SITE: Dome C, Antarctica

Dome C site, Antarctica, is one of the best site for millimetre and submillimetre astronomy on Earth thanks to its low value of **Precipitable Water** Vapour (pwv)

1.2

1.0

0.2 0.0 (mm) ^{MMd} 0.1

0.0

(mm) vwq 0.8 0.6



Conclusions

QUBIC Analysis

Analysis relate to the necessity of shielding the QUBIC experiment in order to reduce unwanted radiation coming from different contamination sources



The analysis has been realized with the support of the simulation software *GRASP* (General Reflector and Antenna Software Package) developed by TICRA Corp.

Goal of this analysis is the determination of the best geometrical configuration for the forebaffle and ground shield that should be installed in the QUBIC experiment

Study of the beam pattern of the instrument including sidelobes concerning spillover contributions

ARS



All the simulations have been performed using the MultiGTD approach (i.e. Geometric Theory of Diffraction) suitable when the dimensions of the reflectors are thousandths times of wavelength



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QUBIC Beam

Beam pattern analysis

Circular shape feed horn array Feed horn array 400 back to back (B2B) feed horns (total diameter = 300 mm)

Hybrid conical horn



Each horn has been modelled with *GRASP* by a Hybrid Conical Horn with following parameters:

- i. waveguide diameter = 4 mm
- ii. horn diameter dh = 12.3 mm
- iii. FWHM = 14 degrees
- iv. centre to centre distance = 13.8 mm



QUBIC Beam

CMB Polarisation

Single horn beam pattern

QUBIC

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Conclusions



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Outline

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CMB Polarisation QUBIC QUBIC Beam ARS

Conclusions

400 feed horns

CMB

Outline



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QUBIC

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Conclusions

QUBIC Shielding

In order to reduce spurious radiative contributions inside the QUBIC focal plane, have been investigated different solutions to correctly select the number and the geometry of the shields for the QUBIC experiment

Forebaffle (FB)

- Fixed on cryostat's window 100 mm above feed horn array
- Conical shape with aperture angle equal to 2*FWHM of single horn = 14°
- 350 mm base diameter and 500 mm height (TBD) has been investigated

Simulations have been performed considering reflective inner surface of the FB , other possible configurations are under investigation



Forebaffle (FB) QUBIC Cryostat



theta(deg)

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Conclusions

QUBIC Shielding

Central feed horn beam pattern (cut @ 0 deg) with and without the presence of the FB



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QUBIC Shielding

Beam pattern central feed horn Central feed horn beam pattern (cut @ 0 deg) for different FB cut @ 0° FB 0.5m FB 1m FB 2m heights (aperture angle = 14°) -20 Amplitude(dB) -40 Increasing FB height, the horn beam pattern -60experiences a cut-off a lower angles from boresight -80-100-100100 ()Increase the FB height over 1 meter is not useful theta

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QUBIC Shielding

Central feed horn beam pattern (cut @ 0 deg) obtained varying FB aperture angle (FB 1 meter height)

14° aperture angle seems to be the good

compromise



CMB CMB Polarisation

tion QUBIC

ARS Conclusions

QUBIC Shielding

In order to minimize the loading coming from the ground and picked up from the instrument, for QUBIC experiment has been planned the realization of a Ground Shield (GS) fixed on the ground



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QUBIC Shielding

Central feed horn beam pattern (spherical cuts @ 0 and 90 degrees) for the only FB and for the FB including GS at zenith position (i.e. varying the FB angular position inside the GS will have a different and asymmetric pattern)

The cuts-off (knees) experienced by the beam pattern at ± 90° is given by the presence of the GS (the Grasp analysis has to be better modelled)



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QUBIC Shielding

Possibility to implement QUBIC shielding including a new shield in-built with the cryostat: Elizabethan Collar (EC) (i.e. in analogy with the veterinarian medical device)

Elizabethan Collar(EC)

- Conical shape with aperture angle of 28°
- 500 m base diameter (TBD) 100 mm up to the feed horn array
- Fixed on the cryostat with a inner reflective surface







Outline CMB CMB Polarisation QUBIC ARS Conclusions
QUBIC Shielding



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Conclusions

QUBIC Spillover

Spillover contributions estimated for the 3 main contamination sources surrounding QUBIC experiment

Scan strategy: QUBIC will scan the sky from the zenith position to a minimum elevation equal to 35° (TBD), with an azimuth position diametrically opposite to the Sun and Moon

Evaluation of the spillover contributions on the entire detectors focal plane (efficiencies have not been included) in terms of temperature

 $S(z) = \frac{\int_{\Delta\theta} \int_{\Delta\phi} T(\theta,\phi) AR(\theta,\phi) sin\theta d\theta d\phi}{\int_{\Delta\theta} \int_{\Delta\phi} AR(\theta,\phi) sin\theta d\theta d\phi}$



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Conclusions

QUBIC Spillover

Spillover evaluation related to the presence of the Ground (T=300K, emissivity=1) Vertical line indicates the maximum zenithal angle reached during QUBIC sky scan (TBD)

Black curve: central feed horn main beam pattern (see slide 17) Red curve: central feed horn beam pattern including FB (see slide 21)

Ground spillover @ zenithal position:

- 627 mK no FB
- 111 mK with FB



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Conclusions

QUBIC Spillover

Spillover evaluation related to the presence of the Sun (T=6000K, angular diameter = 30 arcmin), (@ horizon, opposite azimuth position)

Vertical line indicates the maximum zenithal angle reached during QUBIC sky scan (TBD)

Black curve: central feed horn main beam pattern (see slide 17) Red curve: central feed horn beam pattern including FB (see slide 21)

Ground spillover @ zenithal position:

- 3 mK no FB
- 328 μ K with FB

$$S(z) = \frac{\int_{\Delta\theta} \int_{\Delta\phi} T(\theta,\phi) AR(\theta,\phi) sin\theta d\theta d\phi}{\int_{\Delta\theta} \int_{\Delta\phi} AR(\theta,\phi) sin\theta d\theta d\phi}$$

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Conclusions

QUBIC Spillover

Spillover evaluation related to the presence of the Sun (T=135K, angular diameter = 30 arcmin), (@ horizon, opposite azimuth position)

Vertical line indicates the maximum zenithal angle reached during QUBIC sky scan (TBD)

Black curve: central feed horn main beam pattern (see slide 17) Red curve: central feed horn beam pattern including FB (see slide 21)

Ground spillover @ zenithal position:

- 70 µK no FB
- 111 μ K with FB

$$S(z) = \frac{\int_{\Delta\theta} \int_{\Delta\phi} T(\theta, \phi) AR(\theta, \phi) sin\theta d\theta d\phi}{\int_{\Delta\theta} \int_{\Delta\phi} AR(\theta, \phi) sin\theta d\theta d\phi}$$

ARS



CMB Polarisation

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on QUBIC

Conclusions

ARS

QUBIC Spillover

Same analysis has been conducted considering the presence of the Ground Shield (see slide 25).

The GS presence more reduces the spillover contributions due to the 3 main sources considered, the values obtained when QUBIC observes the Zenith are:

Ground = 2mk Sun = $7\mu K$ Moon = $0.1\mu K$

The same analysis has been realized to estimate the spillover contribution picked-up by the central pixel on the focal plane, in this case has been assumed, as instrument pattern $AR(\vartheta, \varphi)$, the synthesized beam (see slide 18) with a cut at $\pm 9^{\circ}$ due to detector array size (no shields are included)

Ground = 44mk Sun = $147\mu K$ Moon = $3\mu K$





To define the acceptable amount of the spillover, we keep in mind the following constrains:

- the radiative loading on the detectors focal plane coming from each feed pattern
- the faint sky signal (in terms of temperature) that will be detect



Necessity to analyze different geometries for the FB and the GS to reduce as much as possible spillover contaminations (including also the possibility to realize the Elizabethan Collar)

Outline **CMB** Polarisation Conclusions CMB QUBIC ARS **QUBIC Atmo**

 \checkmark To correctly select the right number and the best geometry for the shields realization is necessary to put attention on treatment of the radiative loading incoming on the pixels of the focal plane given by the atmosphere, and to compare it with the ground pick-up

The radiative loading (in terms of power) coming from atmosphere, varying the pointing direction, can be expressed in the following way

$$P_{atmo}(z) = \frac{1}{2} \Delta \nu A_h N_h t_{tot} \epsilon_{opt} \int_{\Delta \theta} \int_{\Delta \phi} GB(\theta, \phi) B(\theta, \phi) sin\theta d\theta d\phi \qquad z = \text{zenithal angle} \quad \Delta \nu = 37.5 \text{ GHz}$$

$$A_h = 5.9 \text{ cm}^2 \qquad N_h = 400$$

$$t_{tot} = 0.59 \qquad \varepsilon_{tot} = 0.2$$

 $GB(\vartheta, \varphi) = BB(T_{atmo} = 240K)\varepsilon(z, pwv)$ Atmospheric Brightness

 $\mathcal{E}(z, pwv) = 1 - e^{-\tau_0(pwv, \Delta v)\operatorname{sec}(z)}$ **Atmosferic Emissivity**

Opacity

$$\tau_0(pwv, \Delta v) = (a_0 + a_1 \Delta v / v) + (b_0 + b_1 \Delta v / v) pwv^{(*)}$$

(*) De Gregori et al. MNRAS 2012

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1.0 pwv (mm) 1.5

2.0

0.5

0.02 0.01

0.0

Opacity vs Precipitable Water Vapour (*pwv***)**

ما حمد ما حاد







Earth's spillovers contribution is always lower than 4 pW for all the QUBIC pointing position (N_{pixel} =992)

Conclusions

ARS

QUBIC Atmo

Power collected by the central pixel considering both unwonted sources, Atmosphere and Earth

The Atmosphere emission has the major impact in the radiative loading budget

CMB

The power collected by a single pixel (the central in the analysis) is always below the expected saturation limit (20 pW TBD) for the QUBIC detectors even under the worst *pwv* conditions (2 mm)

central pixel $0.4 < P_{atmo}$ (pW) < 1.4 for 0.1 < pwv < 0.4 @ zenith

The power collected by a single pixel from Earth is $4~{\rm fW}$ (without FB) reduced to $0.1~{\rm fW}$ including the FB

Next steps:

- i. define the maximum acceptable loading on detectors (TES saturation limit)
- ii. Realize with GRASP the synthesized beam including the presence of the shields
- iii. realize a ground model emission and a model to take account atmospheric fluctuations



Conclusions

Anti-Reflection Structures

The realization of optical refractive devices at millimeter and sub-millimeter wavelengths is focused to reduce the loss of the incident radiation by reflection. Fresnel reflection causes the loss of portion of the radiation incident power to be back reflected from an interface

decrease of the throughput of the optical system

 In millimetre band is basic increase the collection of the incoming radiation especially in CMB
 Polarisation experiments, like QUBIC and LSPE (Large Scale Polarization Experiment), due to the small intensity of this kind of cosmological signal

Anti-Reflection Coating (ARC) is the most employed technique to suppress Fresnel reflection, which consists by coating the optical element with one or more polymeric material layers or meta-materials, using the interferential behavior of the radiation inside the coating to shrink reflection

Disadvantages for mm optical devices

- thermal performances (adhesion an stability) @ cryogenic temperatures
- high realization costs

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ARS

QUBIC

ARS

Conclusions

Anti-Reflection Structures

Anti-Reflection Structures (ARS) is an alternative technique to reduce Fresnel reflection, originally developed for visible and infrared optical system, based on the mechanical manufacturing of the optical element surface anti-reflection behavior due to the variation of the refractive index of the dielectric material depending on geometrical configuration of the worked surface (Priciples of Optics, Born & Wolf)

Biological inspiration

CMB

discovered by studying the geometrical shape of the cornea of night-flying moths (M. C. Hutley et al., Nature, 244, 281, 1973)

Grating Diffraction Geometry

As a typical grating, the ARS are realized to propagate only the reflected and transmitted Oth orders (higher diffraction orders are evanescent) (Quasioptical System, P. Goldsmith)

 $\begin{array}{ll} n_2 \sin \theta_m - n_1 \sin \theta_i = \frac{m\lambda}{\Lambda} & \text{grating equation} \\ n_2 \text{substrate refraction index} & \Lambda & \text{grating period} \\ n_1 \text{Incident medium refraction index} & \theta_m \text{angle of } m \text{th order} \\ \lambda & \text{incident free-space wavelength} & \theta_i & \text{angle of incidence} \end{array}$

 $\frac{1}{\lambda} \le \frac{1}{\max[n_2, n_1] + n_1 \sin \theta_{\max}}$

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period to wavelength ratio



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CMB Polarisation

QUBIC

Conclusions

HFSS Simulations



 Possibility to apply this kind of technique also @ mm and sub-mm wavelengths, in order to extend its application in many future astrophysical and cosmological experiments

ARS

Low realization costs

HFSS = High Frequency Structure Simulator by Ansoft Corporation vers 13.0

analyze the electromagnetic behavior of the three-dimensional structures using the finite-elements analysis to solve the Maxwell's equations







Results from HFSS simulations

- i. Starting from 4% reflectivity, derived by Fresnel equation for a smooth HDPE slab, the simulations show how the ARS allow to reach a reflectivity lower than 0.4%
- ii. Best performance are obtained with the spherical configuration
- iii. Presence of spurious polarization component (upper right plot), manly for incident angles greater the 20°; this effect must be taken into account concerning the use of the ARS in polarization experiments

Next step will be the realization of the first ARS prototype to realize the experimental measurements tanks to validate the results obtained by simulations

Outline CMB CMB Polarisation QUBIC ARS Conclusions

• Bolometric Interferometry:

a new approach for B-modes quest

• QUBIC Experiment

shielding analysis with GRASP

Anti-Reflection Structures @ mm band
 innovative realization technique

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